

Problem 2 Pop-Pop Boat

Shantanu Kadam, Shirley Yu
String Bean Theorists
UC Berkeley

Prompt

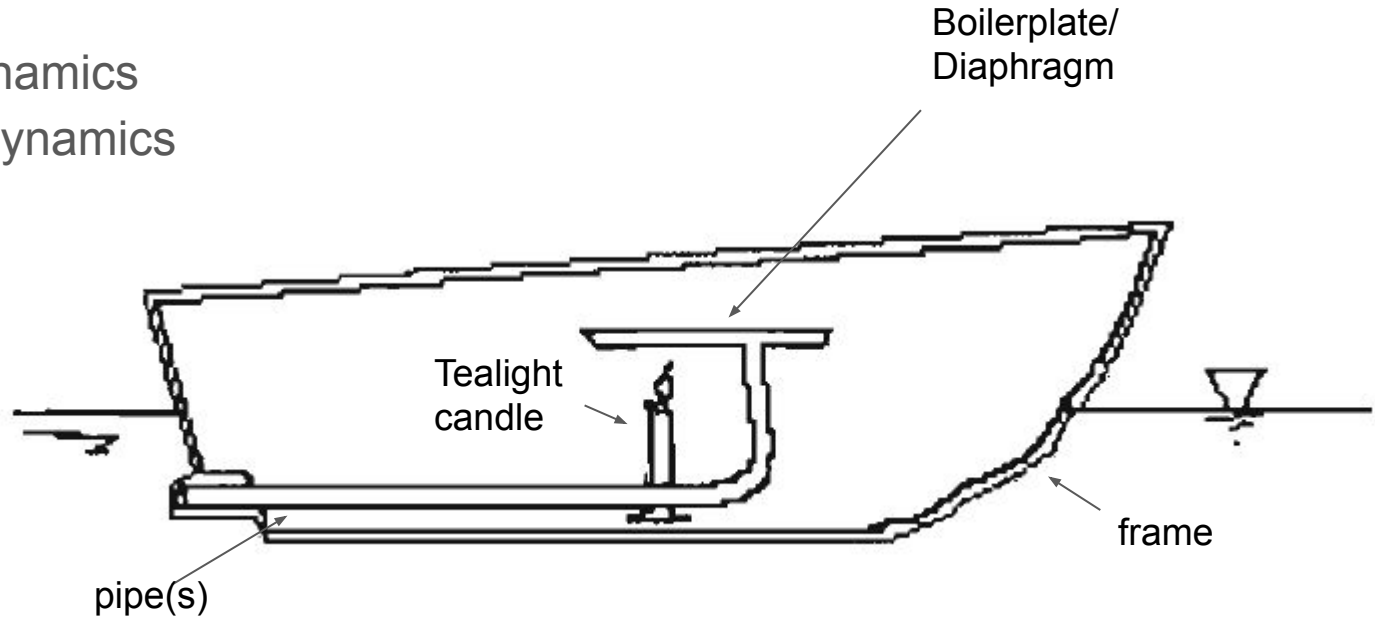
The Pop-Pop boat is a small toy powered by a candle. Its engine is very simple, since it is just made of a boiler.

1. Propose a boat design that **maximizes the travelled distance** using a tealight candle.
2. Estimate the **energy conversion efficiency** of your boat. (engine: traveled)



Theory: What is a pop-pop boat?

1. Hydrodynamics
2. Thermodynamics

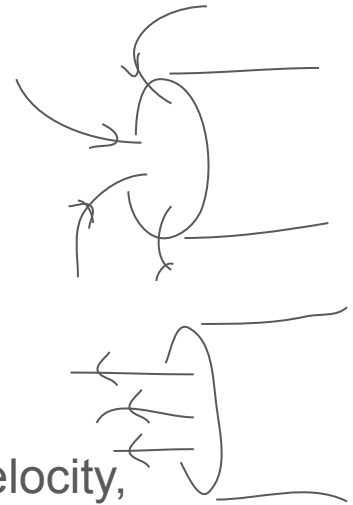


Theory: Hydrodynamics

- 2 phases: suction, exhaust
 - Boat starts w/ water in pipes/boiler, so net mass flux = 0
 - But divergence of inflow greater than outflow \Rightarrow net thrust > 0
 - Due to viscosity & pressure
- By considering momentum conservation at the equilibrium velocity,

$$\langle thrust \rangle = \rho a \langle U_e^2 \rangle$$

Density : ρ
Area of the exit plane : a
Jet velocity : U_e



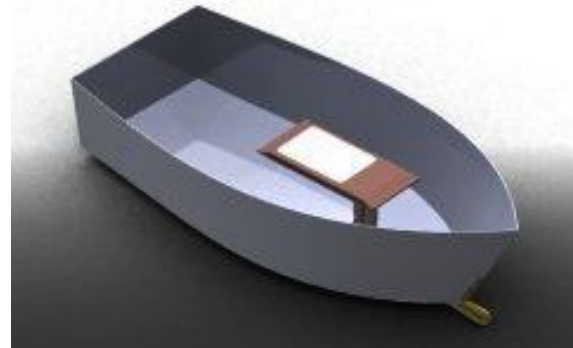
Theory: Thermodynamics

- Candle \Rightarrow steam \Rightarrow pressurizes boilerplate \Rightarrow forces water out of pipes
- Steam travels down pipes to cooler regions \Rightarrow condenses \Rightarrow pressure drops \Rightarrow draws water into pipes

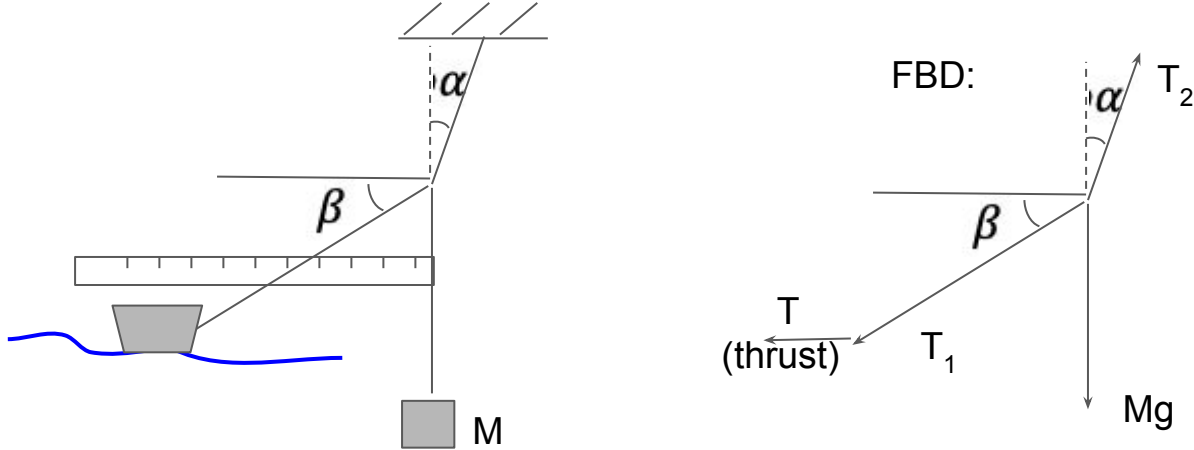
Key Parameters

- No effect
 - putt-putt noise does not affect velocity (e.g. thickening diaphragm)
 - Flexibility of diaphragm (flexible vs inflexible)
- Significant effect (thrust)
 - Number of pipes
 - Length of pipes
 - Jet velocity
 - Jet exit cross-sectional area
 - Reservoir temperature

Experimental Setup: Boat Build



Experimental Setup: Thrust



- Approximate: if α is small (<5 degrees) & $T_2 \ll T_1$ then $T \approx Mg \alpha$
- So run boat and stack weights until equilibrium achieved

Experimental Setups for specific factors

- Introduce bubble into clear pipe extensions w/ high-speeds recording
 - bubble displacement \Rightarrow suction & exhaust velocities, pressure at pipe exit

Data Analysis

1. Work done by boat: $\langle T \rangle = \rho \alpha \langle U_e^2 \rangle$
2. Work done by steam:
 - a. Area under P-V diagram

Future

1. Maximizing distance traveled
 - a. Build actual boat(s) and implement experimental setups
 - i. Geometry of heating region (boilerplate vs coiled)
2. Energy efficiency
 - a. Calculate efficiency for specific boat(s) we build
 - b. Account for energy loss of tealight candle itself?

References

- <https://youtu.be/PKk3w1M4J-4?t=519>
- <https://youtu.be/0ki9Kta8g14>
- Propulsion of the Putt-Putt Boat - 1 by V Sharadha
- Propulsion of the Putt-Putt Boat - 2 by V Sharadha
- “2 cheap means to measure the thrust of a pop-pop engine” by Jean-Yves
-

Hydrodynamic Calculations

Variable description:

Density : ρ

Area of the exit plane : a

Acceleration of the
reference frame : a_{rf}

Volume of the control volume : V

Surface forces : F_s

Body forces : F_b

Velocity of the mass leaving
the control volume : U

Drag force : D

Velocity of the boat : U_x

Jet velocity : U_c

Using the momentum conservation equation,

$$F_s + F_b - \int_V a_{rf} \rho dV = \int_{cs} U \rho U \cdot da + \frac{\partial}{\partial t} \left(\int_V U \rho dV \right).$$

After the boat has attained uniform velocity, along the x-direction,

$$F_b = 0$$

$$F_x = \int \tau da, i = D$$

$$a_{rf} = 0$$

Upon averaging over a cycle of operation,

$$\frac{\partial}{\partial t} \left(\int_V U \rho dV \right) = 0.$$

Using the notation,

$$\frac{1}{T} \int_0^T G dt = \langle G \rangle,$$

the momentum conservation equation becomes,

$$\langle F_{sx} \rangle = \int_{cs} \langle U \cdot i \rho U \cdot da \rangle + \int_{cs} \langle p da \cdot i \rangle.$$

Hydrodynamic Calculations

Variable description:

Density : ρ

Area of the exit plane : a

Acceleration of the
reference frame : a_{rf}

Volume of the control volume : V

Surface forces : F_s

Body forces : F_b

Velocity of the mass leaving
the control volume : U

Drag force : D

Velocity of the boat : U_x

Jet velocity : U_e

During outflow, this equation becomes

$$\int_a \langle U_{e,i} \rho U_{e,i} da \rangle + \int_a \langle p da_i \rangle \rho a \langle U_e \rangle^2.$$

During suction,

$$\int_a \langle U_{i,i} \rho U_{i,i} da \rangle + \int_a \langle p da_i \rangle = 0.$$

Therefore the average drag force $\langle D \rangle \approx \rho a \langle U_e^2 \rangle = \langle thrust \rangle$, under steady-state conditions. Drag can also be given in terms of the drag coefficient C_D , as,

$$D = C_D \left(\frac{1}{2} \rho U_x^2 A \right), \text{ where } C_D \text{ can be obtained from correlations.}$$